

# Barrier Technologies Workshop

## Practical Principles for UltrabARRIER Films

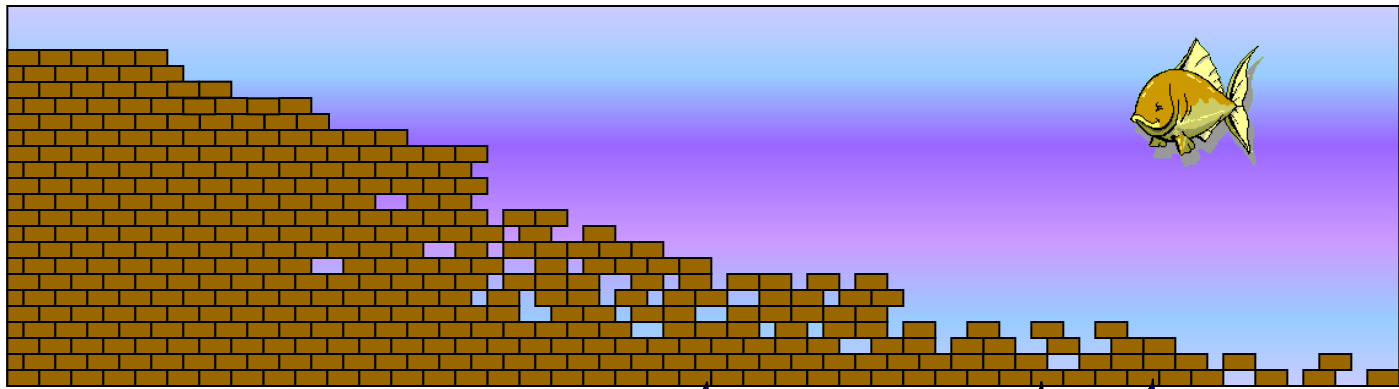
*G.L. Graff, M.E. Gross, P.E. Burrows, W.D. Bennett, C.C. Bonham, P.M. Martin, E.S. Mast, M.R. Zumhoff, M.G. Hall, D.W. Matson, L. Moro, N. M. Rutherford and R.E. Williford*

**Pacific Northwest National Laboratory**

**September 19, 2012**

# The Columbia River Near PNNL





Limit of  
MOCON  
measurement

Note, this is a  
necessary but  
NOT sufficient  
condition as  
display size  
increases

OLED  
Requirement

ULTRA-  
BARRIERS

PECVD  
Inorganic Coatings

Organic Coatings

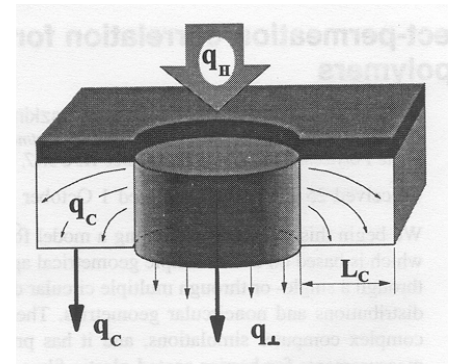
PET (hardcoat)

PNB, Arton

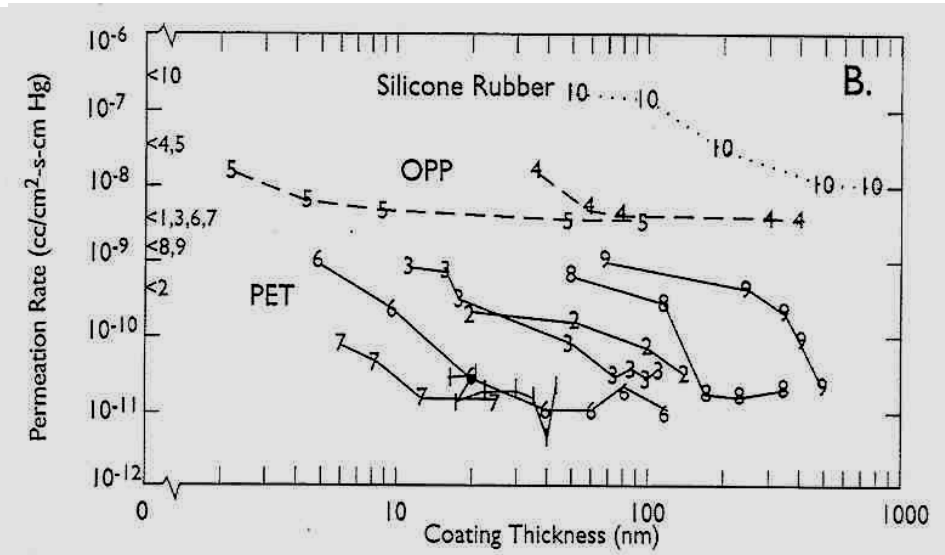
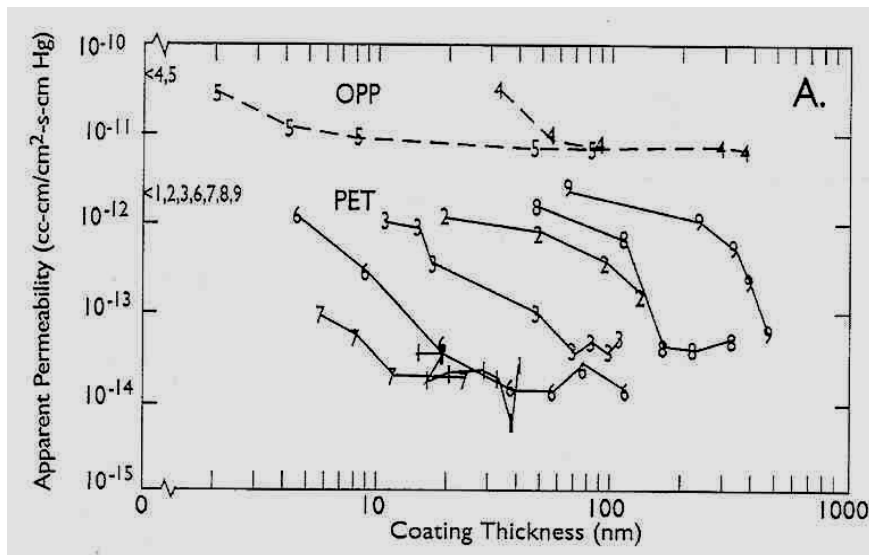
$10^{-6}$        $10^{-4}$        $10^{-2}$        $10^0$        $10^2$        $10^4$

$H_2O$  Permeation Rate (g/m<sup>2</sup>/day at 25°C)

# Defects dominate gas permeation



da Silva Sobrinho, JVST A 18(1),2000

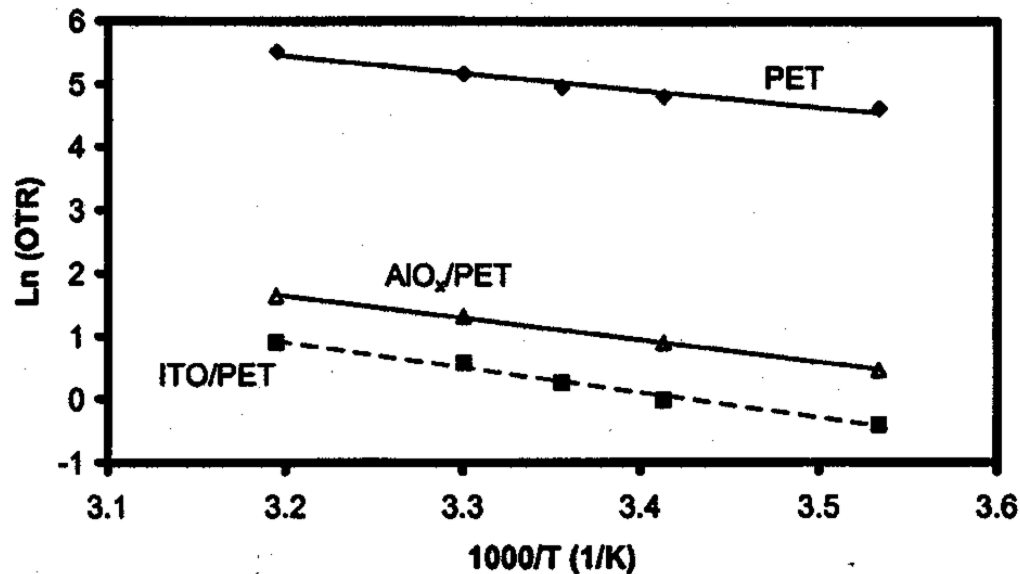


H. Chatham, *Surfaces & Coatings Technology* 78 (1996) 1-9

- *permeation is defect controlled*
- *permeation not following a solubility/diffusivity relation*

# Defects dominate gas permeation

Activated rate theory  $P = P_0 \exp(-E_A/RT)$



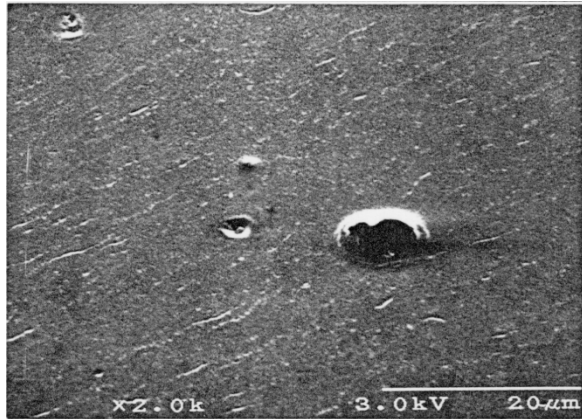
Film type	$E_A$ (KJ/mol $\pm$ 3)
PET	27
PET/AIOx	33
PET/ITO	29

*B.M. Henry et.al., Thin Solid Films 382 (2001) 194*

**Rate controlling mechanism is diffusion of O<sub>2</sub> through PET**

# Thin-film coatings

*Low temperature vacuum deposition leaves defects!*

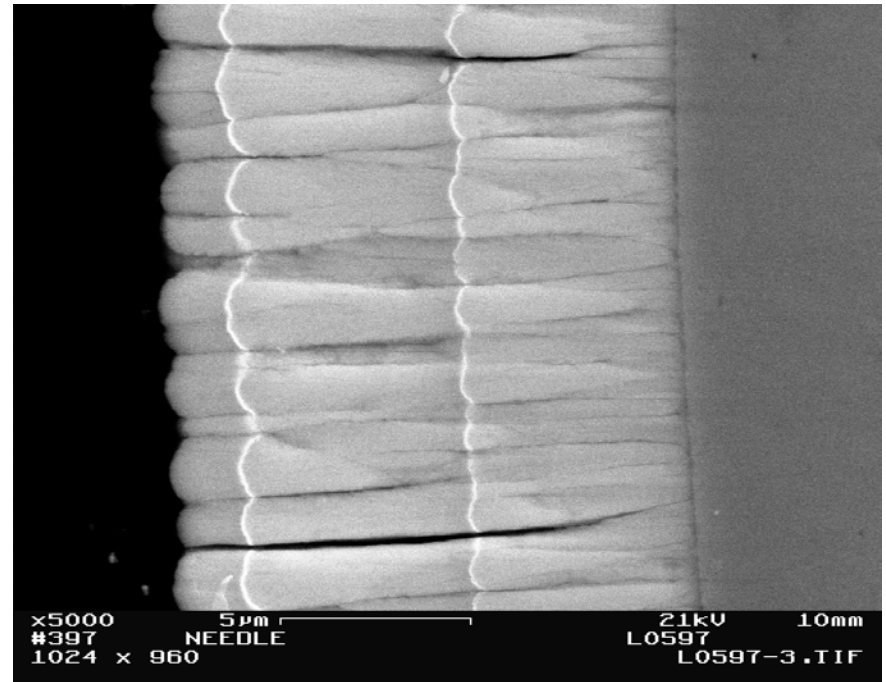


Metallized PP Film (control)



Metallized Acrylate Coated PP Film

Extrinsic



Intrinsic



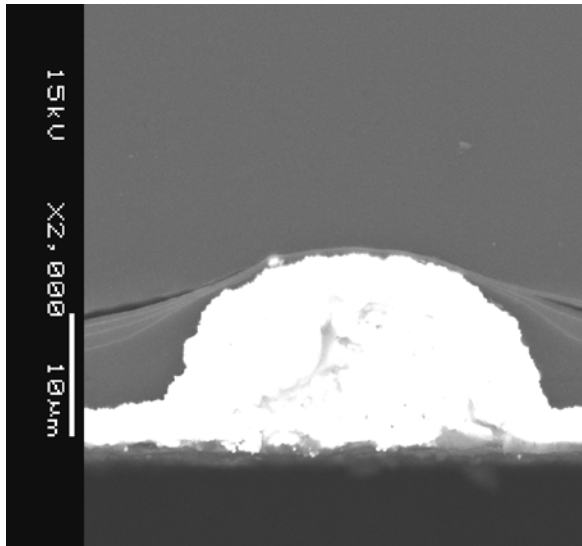
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# Sources of Defects

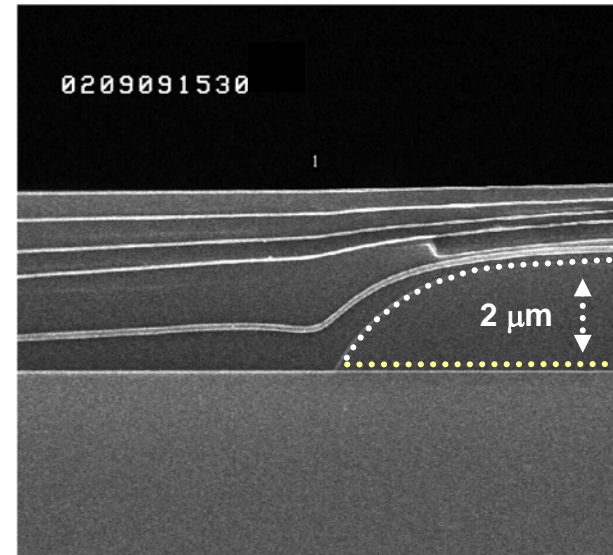
## Intrinsic

- poor deposition (spitting)
- columnar growth
- stress cracking
- grain boundaries
- low density (porous) films

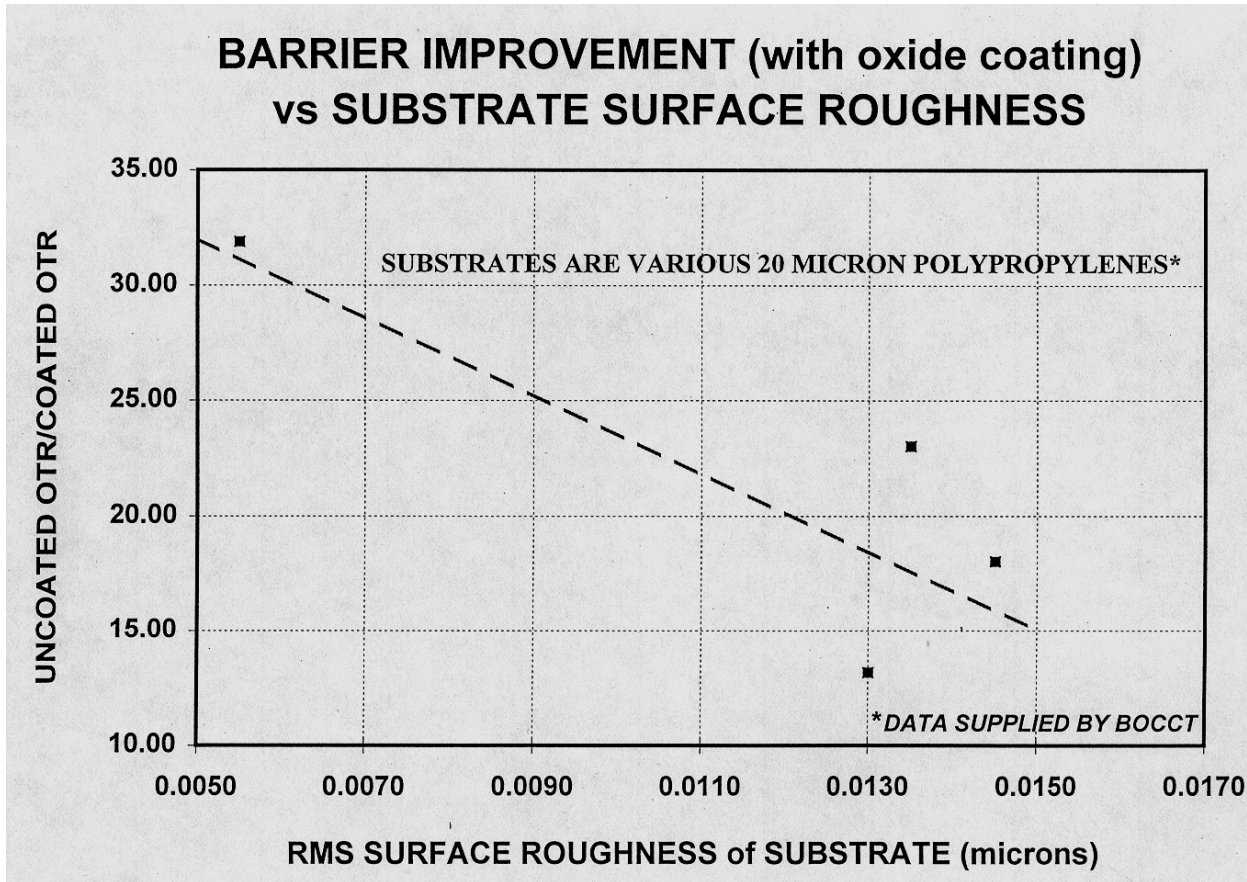


## Extrinsic

- particles / debris
- surface roughness
- topography (step edges)



# Key Requirements for Ultra-Barrier



*Substrate surface roughness generates defects*



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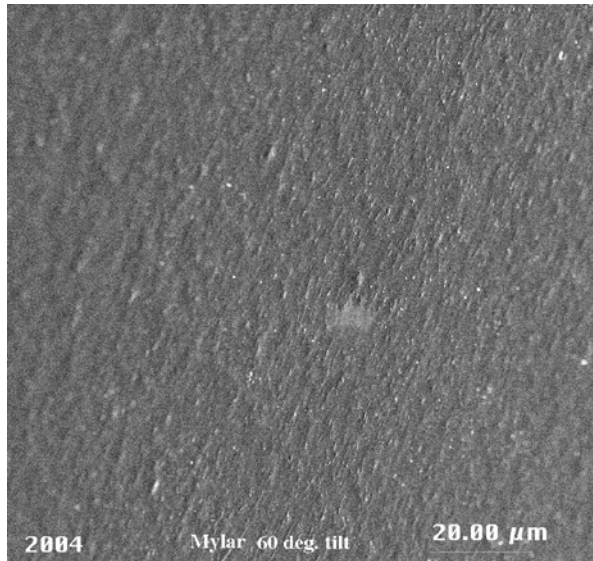
Proudly Operated by Battelle Since 1965



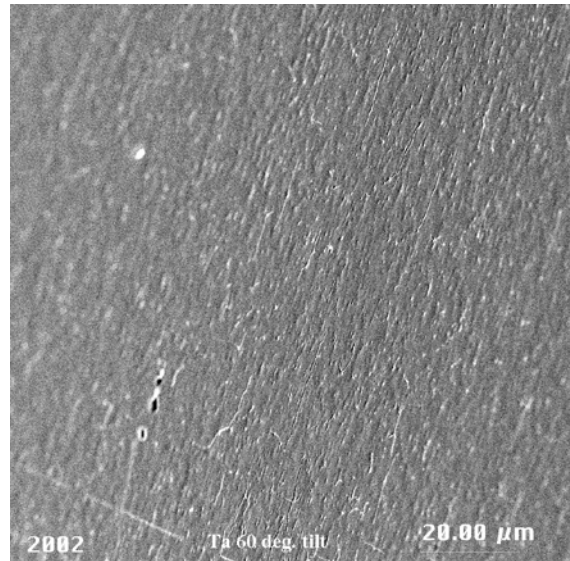
# Key Requirements for Ultra-Barrier

- Surface roughness

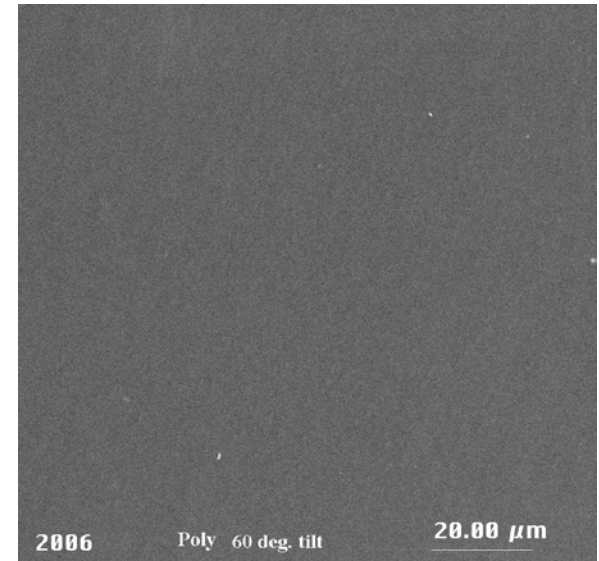
Native PET



Native PET + 25nm Ta



Native PET + 1.5μm poly



*Affinito, et al., Thin Solid Films, 290-91, 63, 1996*

**Conformal** Vacuum PVD/CVD replicate surface features

**Non-conformal** polymer deposition levels surface

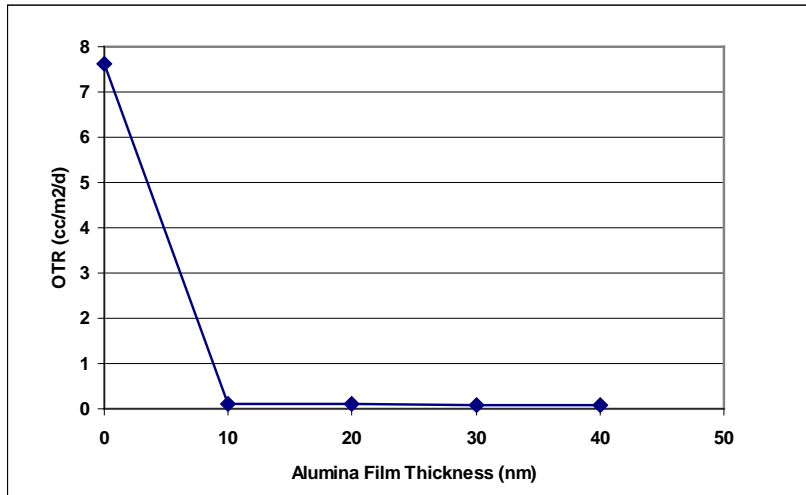


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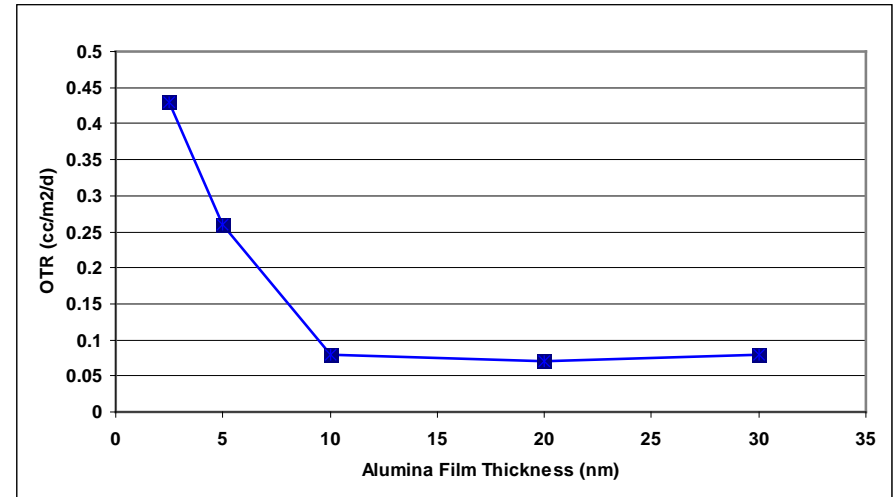
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# Key Parameters for Ultra-Barrier Layers

- critical film thickness required ( $\lambda_c$ )



PNNL barrier on PET



Phillips, R., US# 5,792,550

- ( $\lambda_c$ ) function of deposition process / substrate / barrier chemistry

- ( $\lambda_c$ ) for batch tool = 37.5 nm; for r2r = 52.5nm

*Kapoor, et. al., SVC 505/856 2006*

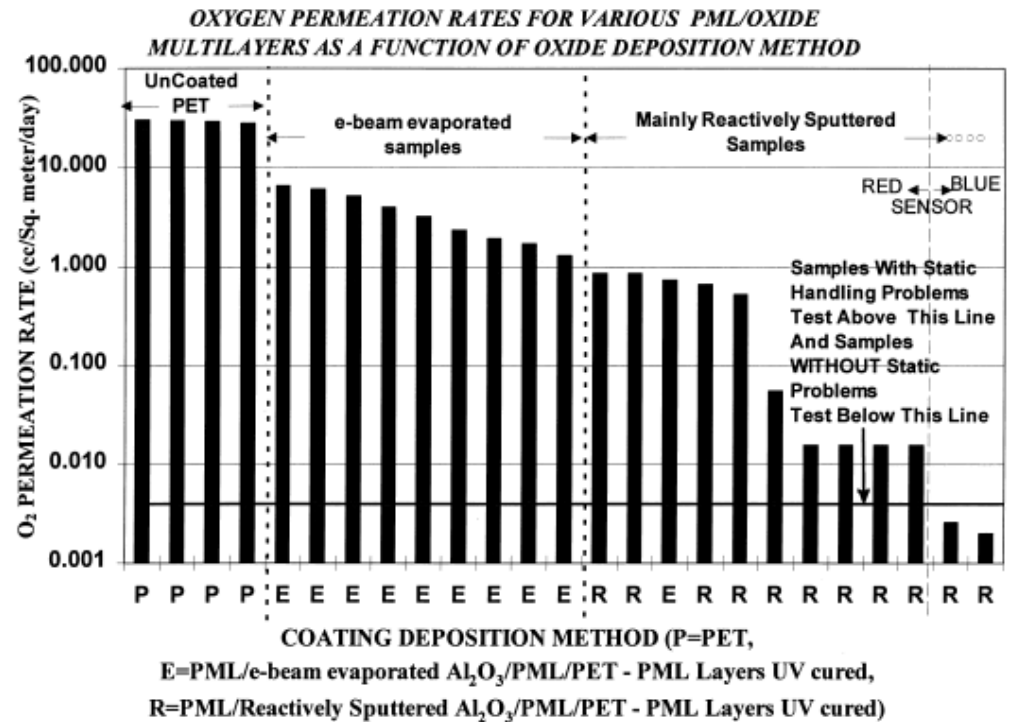
# Key Requirements for Ultra-Barrier

## Deposition process / conditions

Deposition Method	OTR (cc/m <sup>2</sup> /d)
EB-Evaporation	15-70
PE-CVD	4
Sputtering	0.5

Yamada et al., SVC Proc., 28, 1995

40-80 nm SiO<sub>x</sub> on PET



Affinito et al., Thin Sol. Films, 308, 1997

- quality of inorganic film is critical



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# Key Requirements for Ultra-Barrier

## Single layer/dyad performance level

### TEST RESULTS:

SAMPLE NAME		MEASURED VALUE
		cc/100in <sup>2</sup> /24Hours
2/5/99-O2-ITO	A	less than 0.0003 < 0.0005
	B	less than 0.0003 < 0.0005
2/5/99-O2	A	less than 0.0003 < 0.0005
	B	less than 0.0003 < 0.0005

13614-27

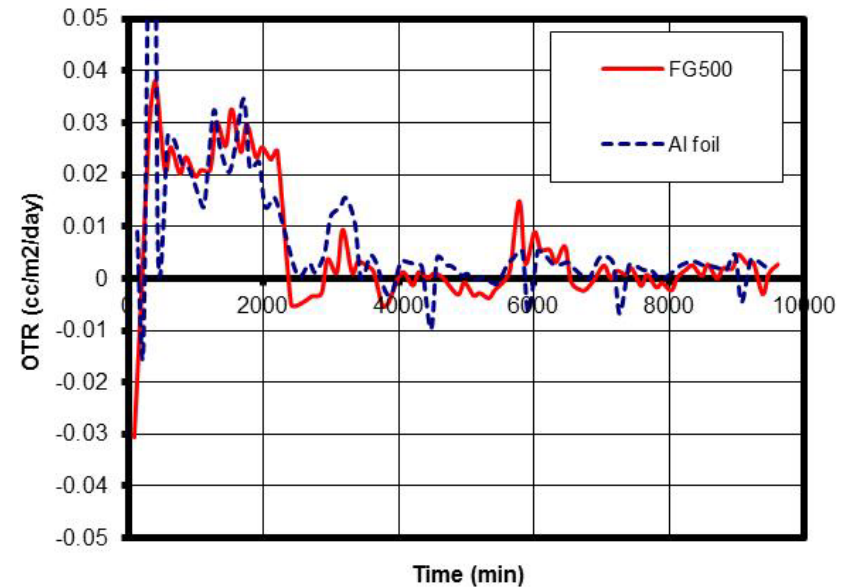
FGT/1.0um Pary/250R/Alon/1.25um Pary

REMARKS: The above samples were tested on a MOCON 2/20 L model Instrument. The lower testing limit of the instrument is 0.0003 cc/100in<sup>2</sup>/24hrs. The above samples were less than this value. Barrier side of samples mounted towards Carrier gas (nitrogen).

Test Operator: Howard Immel

Date: 2-12-99

This information represents our best judgement based on work done, but the company (MOCON) assumes no liability whatsoever in connection with the use of information or findings contained herein.



**Insert into multilayer design**

# ***Key Requirements - Summary***

- ▶ Eliminate / minimize surface roughness
- ▶ Deposit highest quality inorganic layer(s) possible
- ▶ Determine critical thickness for inorganic layer(s)
- ▶ Minimize particulate / debris

***- minimize sources of intrinsic and extrinsic defects!***



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# Understanding Permeation Through Complex Barrier Structures

*J. Applied Physics, 96, 4, 1840 (2004)*

*Flexible Flat Panel Displays, John Wiley & Sons,*

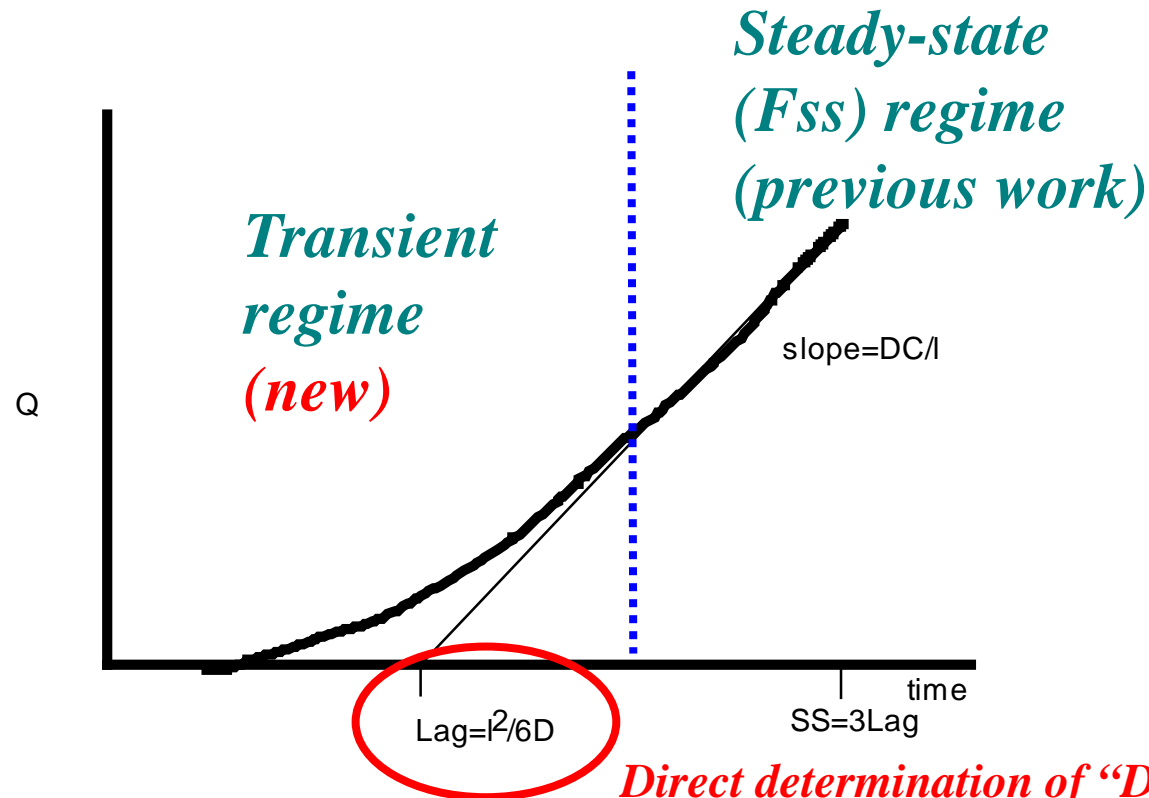
*Gregory P. Crawford (editor), 57-75 (2005)*



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# Mechanisms Approach:



*Single Layer equations*

Lag time =  $l^2/6D$  – calculate diffusivity ( $D$ )

$S = F_{ss} l / (D\Delta P)$  – calculate solubility ( $S$ )

*Direct determination of “D” from layer thickness and gas fluence*

*J. Crank, The Mathematics of Diffusion, 1975*

J. Crank, *The Mathematics of Diffusion*, Clarendon University Press (1975)

- Single layer, concentration profile of vapor as a function of distance and time;  $C(x,t)$ .
- Non-condensable vapor is saturated in the carrier gas at a fixed concentration of  $C_1$  on the “upstream” side of the layer and maintained at zero on the downstream side by a sweep gas, zero initial concentration in the layer.
- Fick’s second law:

$$C(x,t) = C_1 \left( 1 - \frac{x}{l} \right) - \frac{2C_1}{\pi} \sum_{n=1}^{\infty} \frac{1}{n} \sin\left(\frac{n\pi x}{l}\right) e^{-\frac{Dn^2\pi^2 t}{l^2}}$$

- Obtain flux,  $F$ , by differentiation with respect to distance (Fick’s first law).
- Integrate flux at the downstream surface ( $x = l$ ) over time to give the total mass transmitted  $Q$ :

$$Q(t) = \int_{t'=0}^t F(x=l,t') dt' = \frac{DtC_1}{l} - \frac{lC_1}{6} - \frac{2lC_1}{\pi^2} \sum_{n=1}^{\infty} \frac{(-1)^n}{n^2} e^{-\frac{Dn^2\pi^2 t}{l^2}}$$

- As  $t$  becomes large:

$$Q(t \rightarrow \infty) = \frac{DC_1}{l} \left( t - \frac{l^2}{6D} \right) : \text{Permeability} = \frac{F_{ss}l}{\Delta P} = DS$$

steady state flux ( $F_{ss}$ )

Lag time (L)

Solubility (S)



# Approach: Fickian models

*Substitute measured D & S into multi-layer equations for...*

$$F_{ss} = \frac{P_{H_2O}}{\frac{l_1}{D_1 S_1} + \frac{l_2}{D_2 S_2} + \frac{l_3}{D_3 S_3} + \dots + \frac{l_n}{D_n S_n}} \quad \text{Steady state flux (Fss)}$$

$$\text{Lag} = \left[ \sum_{i=1}^n \left[ \frac{l_i}{D_i} \prod_{j=1}^{i-1} K_j \right] \right]^{-1} \left[ \sum_{i=1}^n \left\{ \frac{l_i^2}{2D_i} \sum_{m=1}^n \left[ \frac{l_m}{D_m} \prod_{j=1}^{m-1} K_j \right] - \frac{l_i^3}{3D_i^2} \prod_{j=1}^{i-1} K_j \right\} + \sum_{i=1}^n \left\{ \frac{l_i}{D_i} \prod_{j=1}^{i-1} K_j \sum_{\beta=i+1}^n \left[ \frac{l_\beta}{\prod_{j=1}^{\beta-1} K_j} \sum_{m=\beta}^n \left[ \frac{l_m}{D_m} \prod_{j=1}^{m-1} K_j \right] - \frac{l_\beta^2}{2D_\beta} \right] \right\} \right]$$

*Lag time (L)*

*Ash Barrer & Palmer, Brit. J. Appl. Phys, 16, 884, 1965*

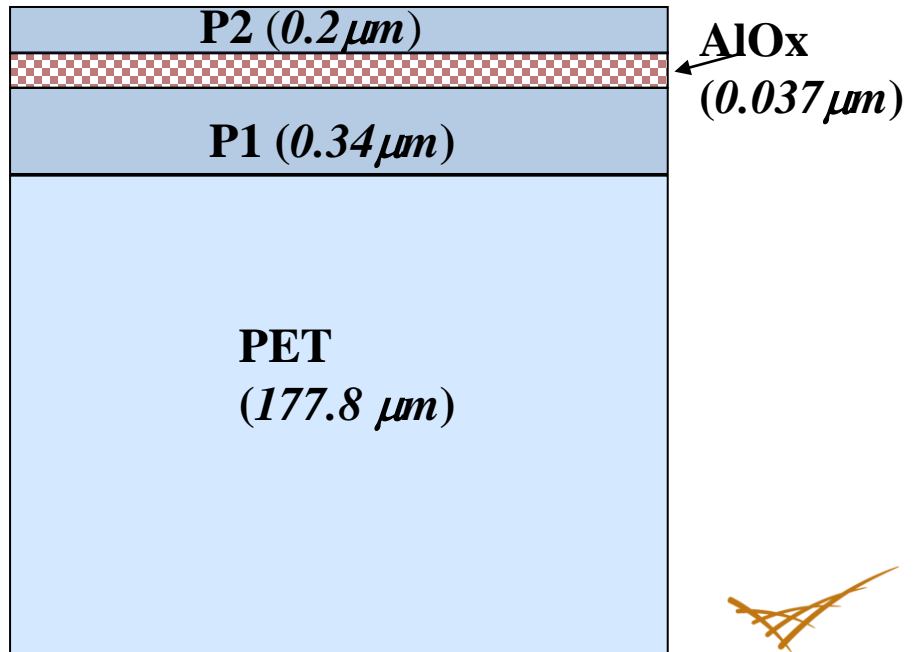
# Our Test Structures:

*combine Mocon measurements  
with Fickian diffusion models*

$$\text{Permeability} = \text{Diffusivity} \times \text{Solubility}$$
$$(P=DS)$$

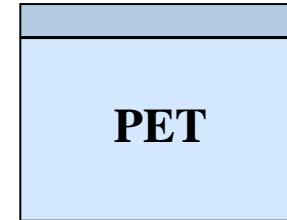
*Need to  
determine  
D & S*

- *use simple structures with known thickness*
  - *PET/P1*
  - *PET/P1/AlO<sub>x</sub>/P2*
- *degas substrate/barrier film*
- *measure fluence as a function of time (Mocon)*

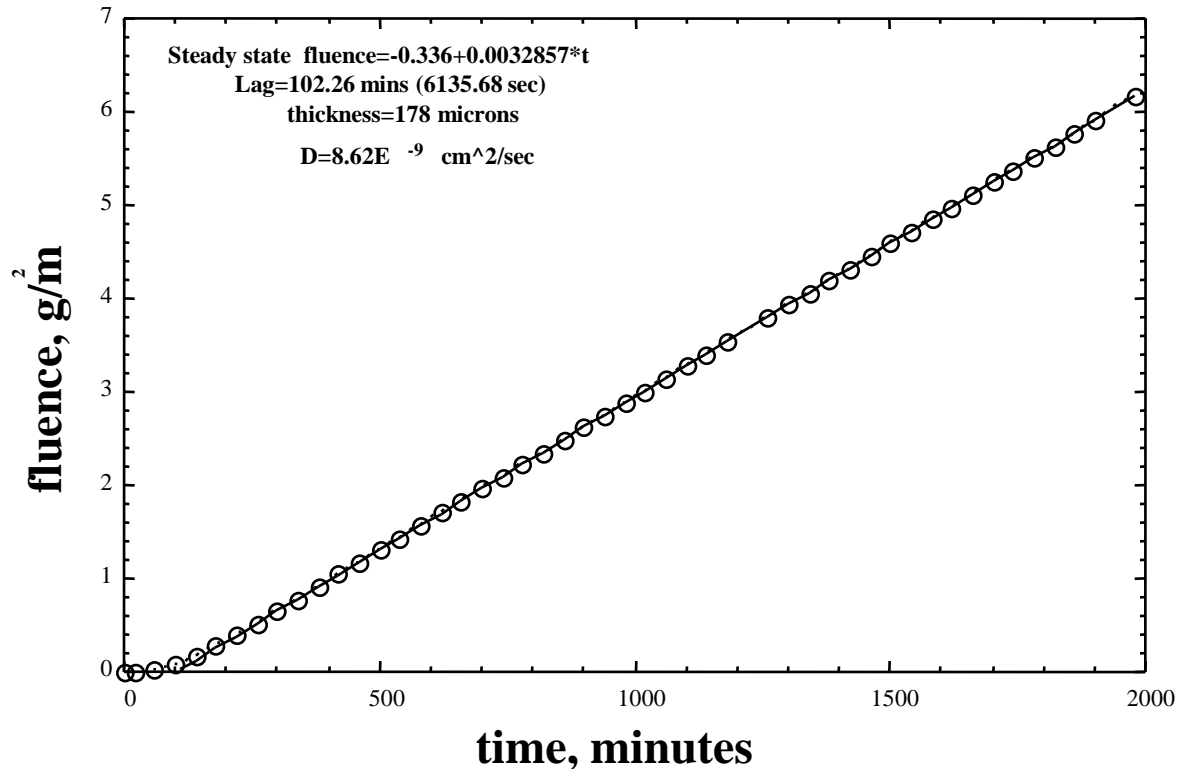


# Barrier Mechanisms

P1



Polymer layers (PET/P1)



$$D = 8.5 \times 10^{-9} \text{ cm}^2/\text{s}$$

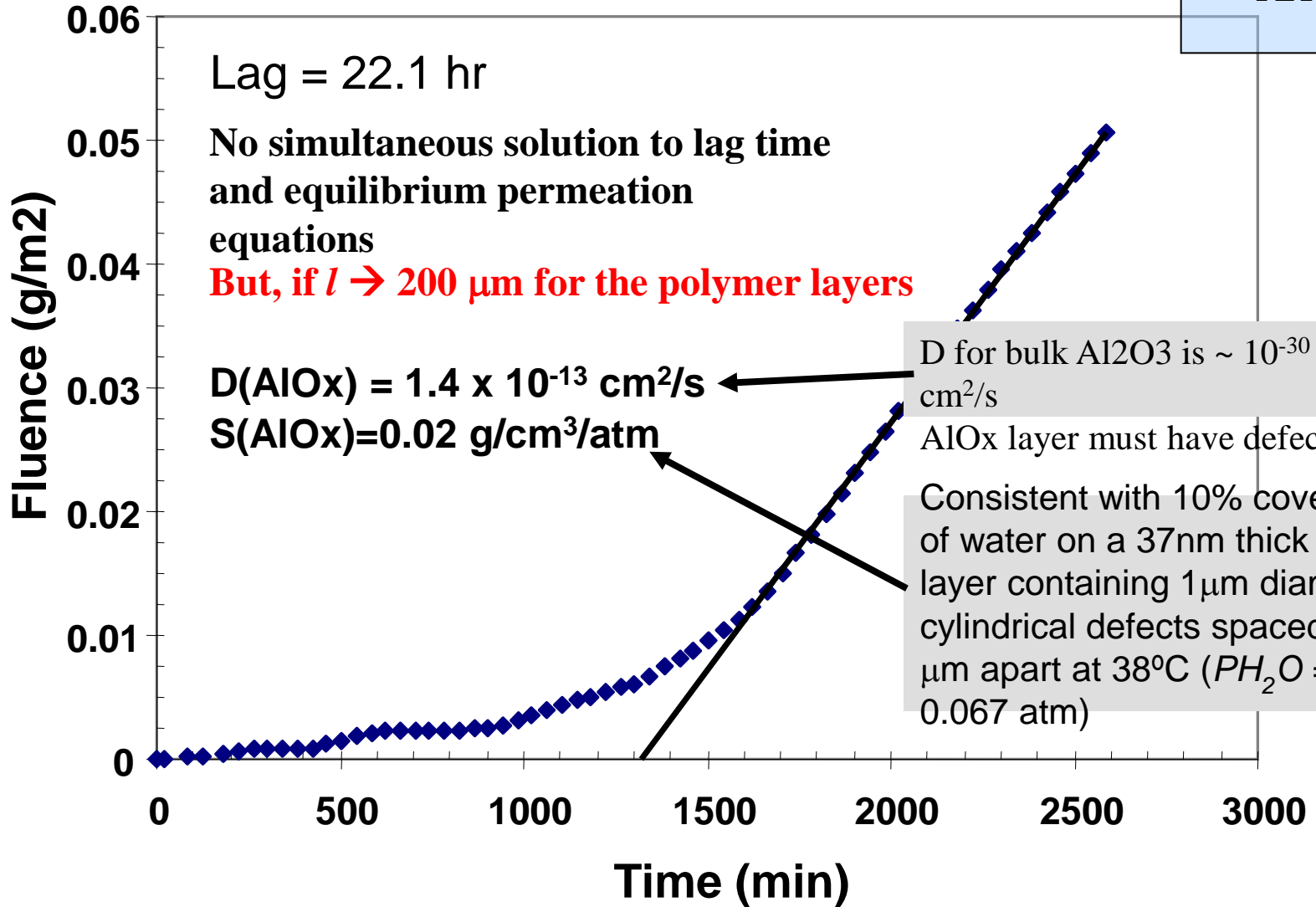
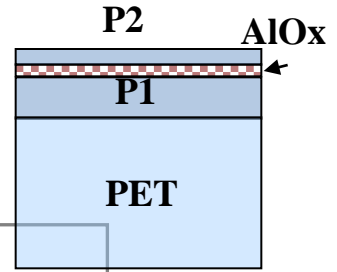
$$S = 0.17 \text{ g/cm}^3/\text{atm}$$



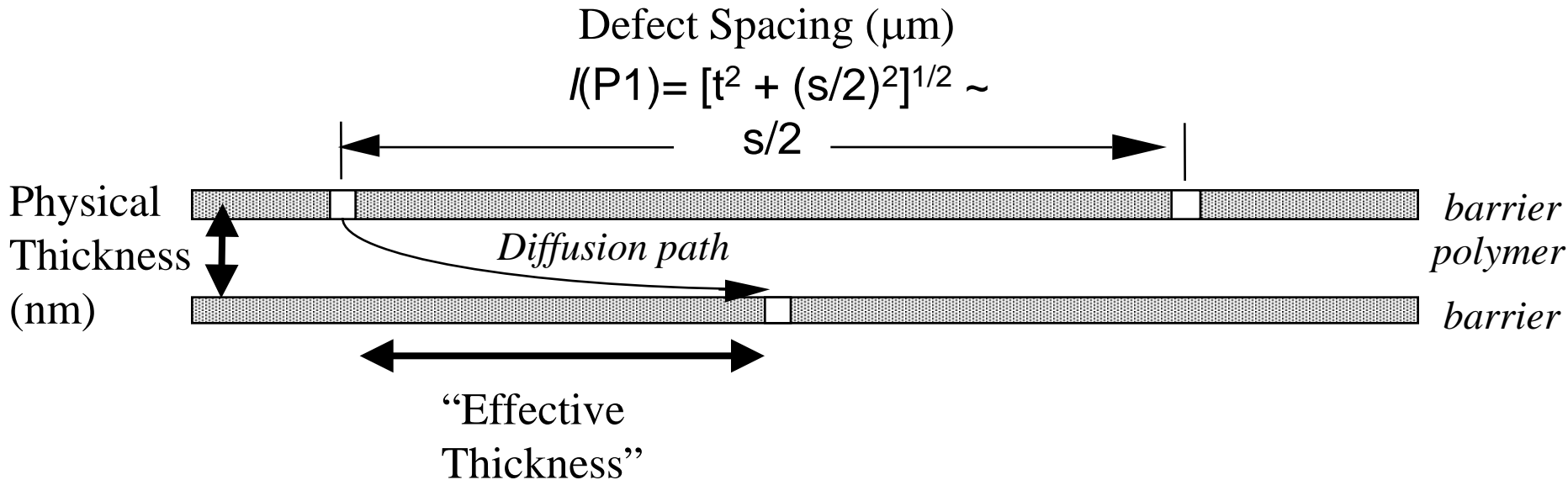
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# Barrier Mechanisms – AlOx layers

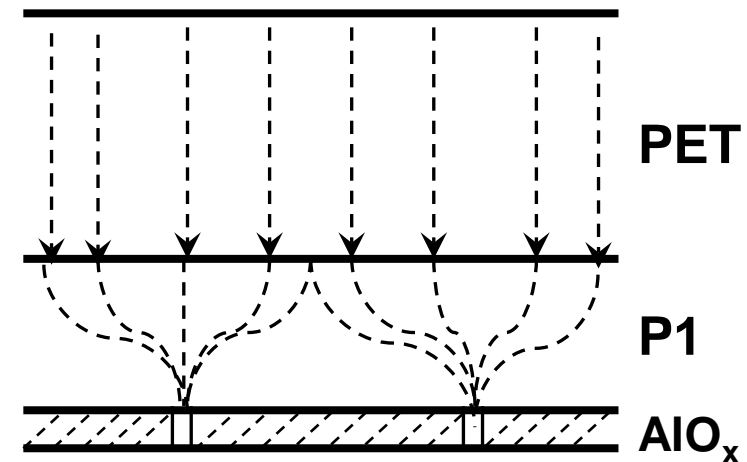


# The Role of Defects in Permeation



*-diffusion of gas in x-y plane dominates*

*-results in extremely long “effective” diffusion path*



# Barrier Mechanism

## *Summary of calculated layer properties*

-  $D(PET)=D(P1)=D(P2) = 8.5 \times 10^{-9} \text{ cm}^2/\text{s}$

- *Handbook values: PET = Acrylic =  $4 \times 10^{-9} \text{ cm}^2/\text{s}$*

-  $S(PET)=S(P1)=S(P2) = 0.17 \text{ g/cm}^3/\text{atm}$

- *Handbook values: PET = 0.17, Acrylic = 0.19*

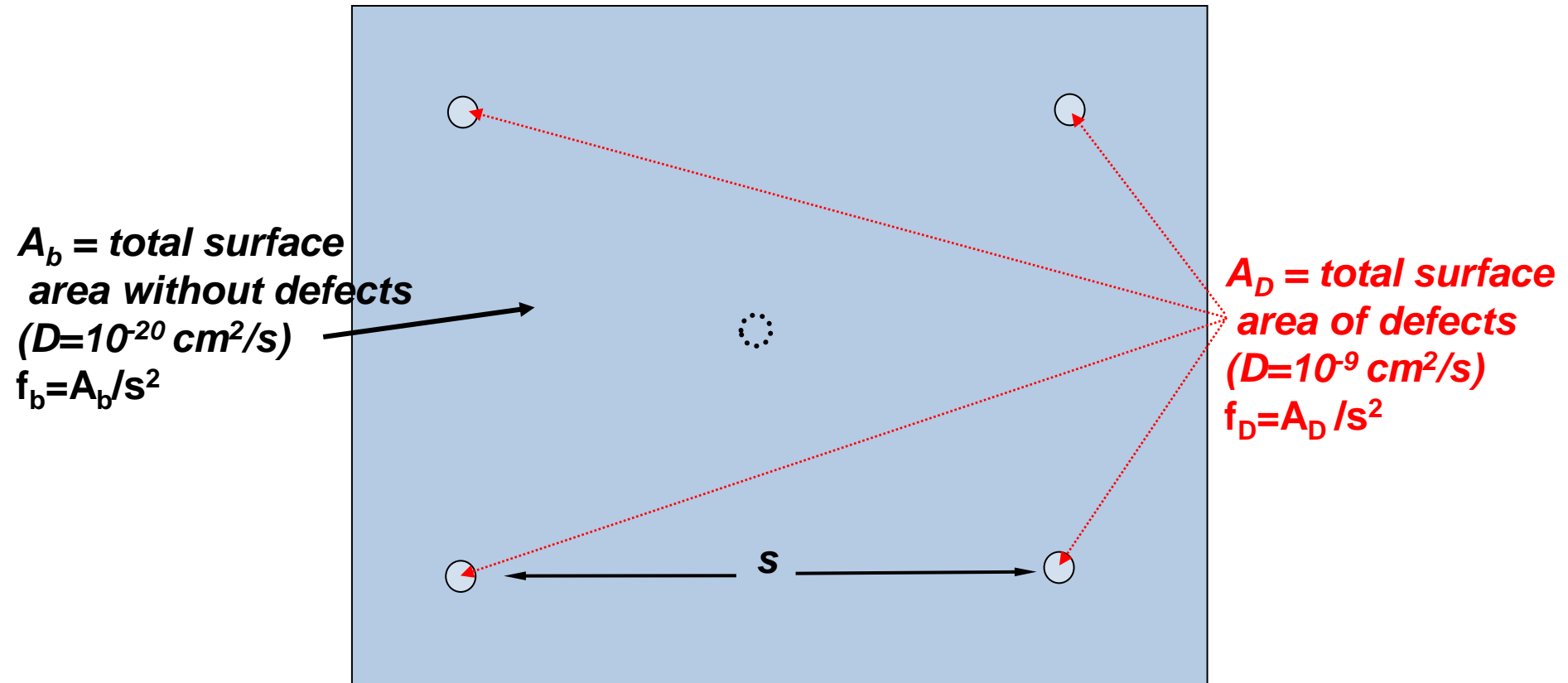
-  $D_{\text{eff}}(\text{AlOx}) = 1.4 \times 10^{-13} \text{ cm}^2/\text{s}$  (sapphire  $\sim 10^{-30} \text{ cm}^2/\text{s}$ )

-  $S(\text{AlOx}) = 0.029 \text{ g/cm}^3/\text{atm}$  (equates to  $\sim 10\%$  surface coverage)

-  $l(P2) = \frac{1}{2}$  defect spacing in AlOx layers (not physical thickness)

# Barrier Mechanisms – Defect model

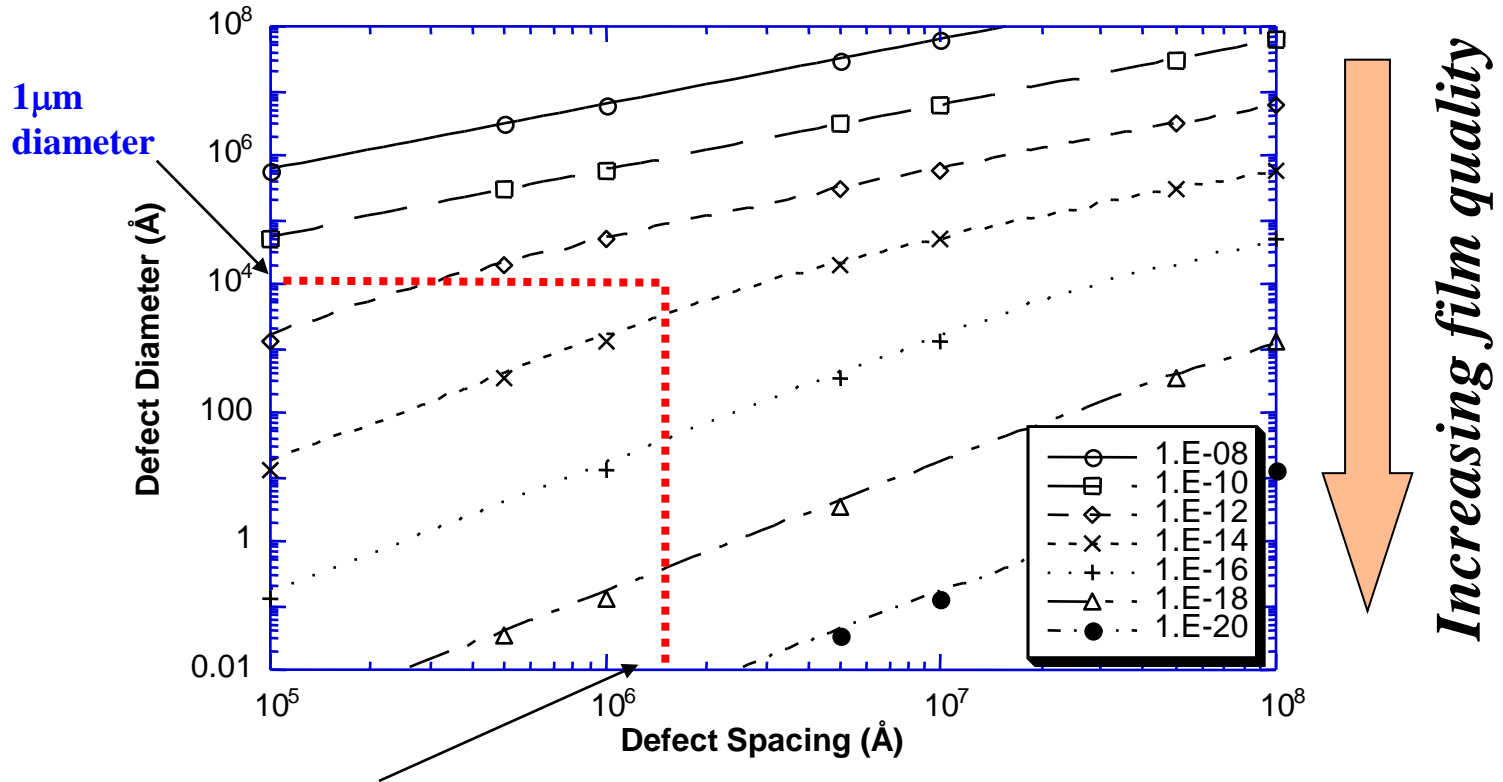
$$D(\text{AlOx}) = D_b f_b + D_D f_D$$



- for  $D_{\text{eff}} = 1.4 \times 10^{-13} \text{ cm}^2/\text{s}$ ,  $A_D:A_b \sim 1:10,000$ ,  $\text{Flux}_D:\text{Flux}_b \sim 5 \times 10^8:1$
- essentially all the gas flux is through the defects

# Barrier Mechanisms – Defect model

$$D(\text{AlOx}) = D_b f_b + D_D f_D$$

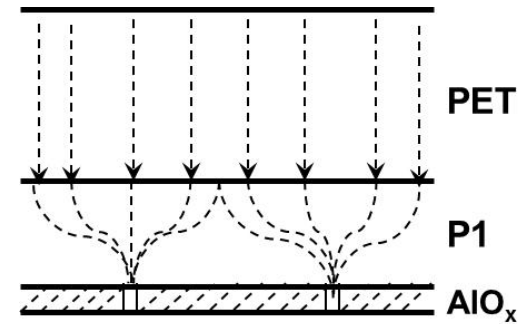
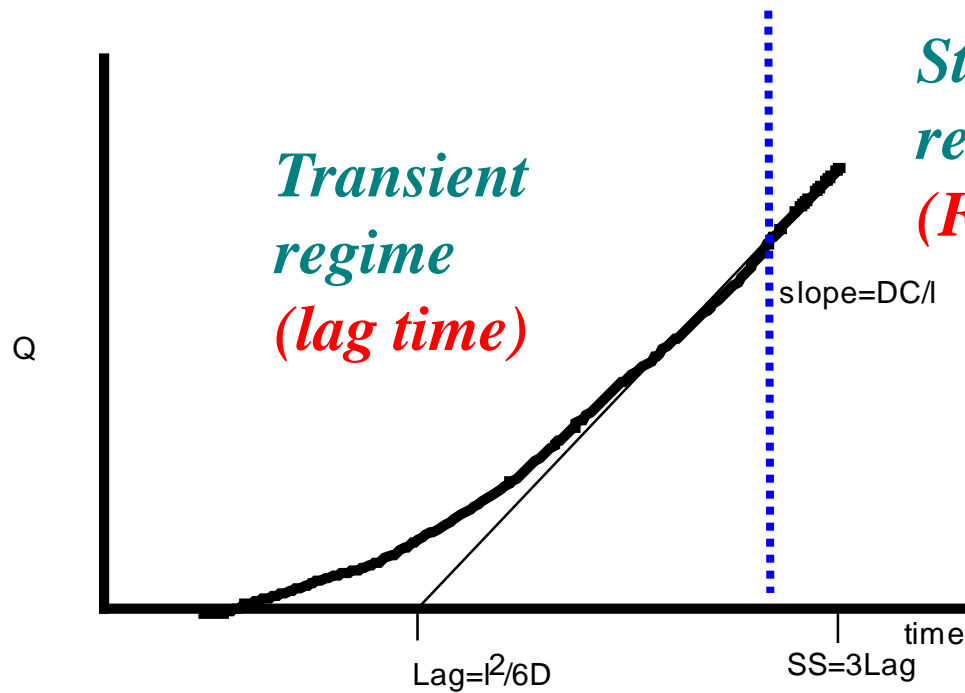


~200 μm spacing between defects @  $D_{eff} = 10^{-13} \text{ cm}^2/\text{s}$



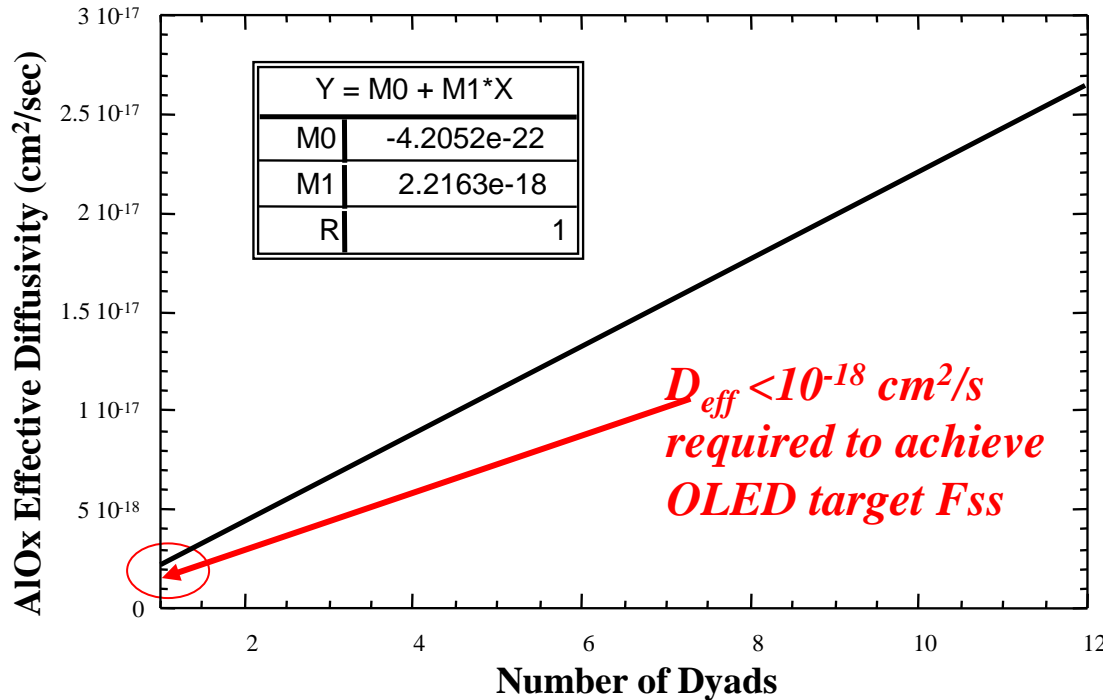
# What do the models teach us?

# Steady State (Single Layer) Regime



# Why not use One Inorganic Layer?

Number of dyads required to achieve  $F_{SS} = 10^{-6} \text{ g/m}^2/\text{d}$



*Very difficult to manufacture using PVD or CVD methods*

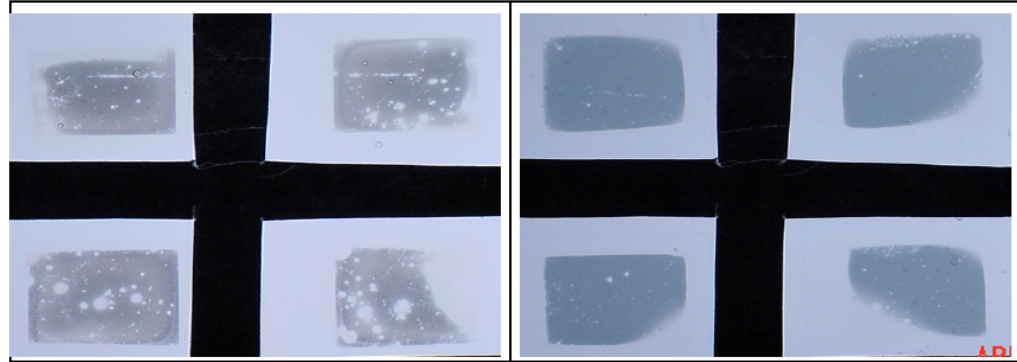
- *equivalent to 1nm defects @ 1000  $\mu\text{m}$  spacing*
- *or 10nm defects @ 10,000  $\mu\text{m}$  spacing*

# Why not use One Inorganic Layer?

## Symmorphix – Magnetron sputtered $\text{Al}_2\text{O}_3:\text{SiO}_2$



- Ca test of pre-cleaned vs. non cleaned PEN after 569Hrs in 60C/90%RH



Pakbaz, H., OSC04 Europe (9/27/2004)

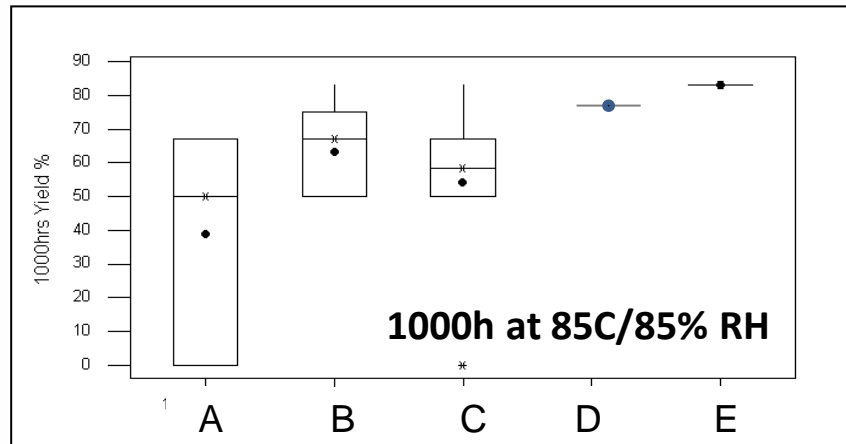
**Measured WVTR of  $1-5 \times 10^{-4} \text{ g/m}^2/\text{d}$**

**25 nm  $\text{Al}_2\text{O}_3$  deposited by ALD: WVTR of  $<1 \times 10^{-5} \text{ g/m}^2/\text{d}$**   
(Zhang, *Thin Solid Films* 517, 2009)



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Condition	Average of 1000hrs WVTR 20/50
A	3.09E-07
B	3.91E-07
C	4.06E-07
E	3.53E-07

## Barrier on PEN sheets

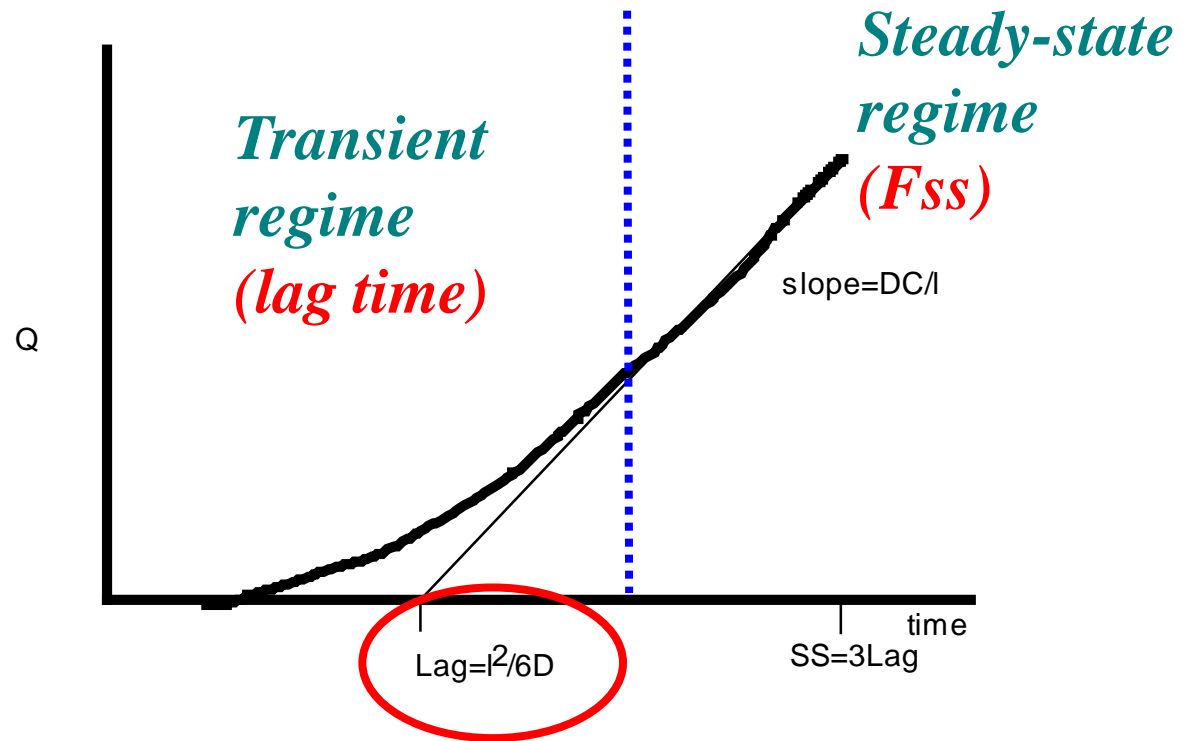
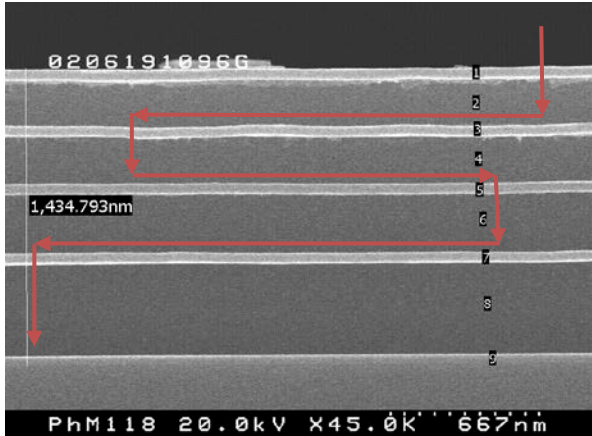
- Typical permeation measured by Ca-test for processes with 100% yield:

- WVTR @ 85/85 =  $2-6 \times 10^{-8}$  g/m<sup>2</sup>-day
- WVTR @ 20/50 <math>< 1 \times 10^{-7}</math> g/m<sup>2</sup>-day



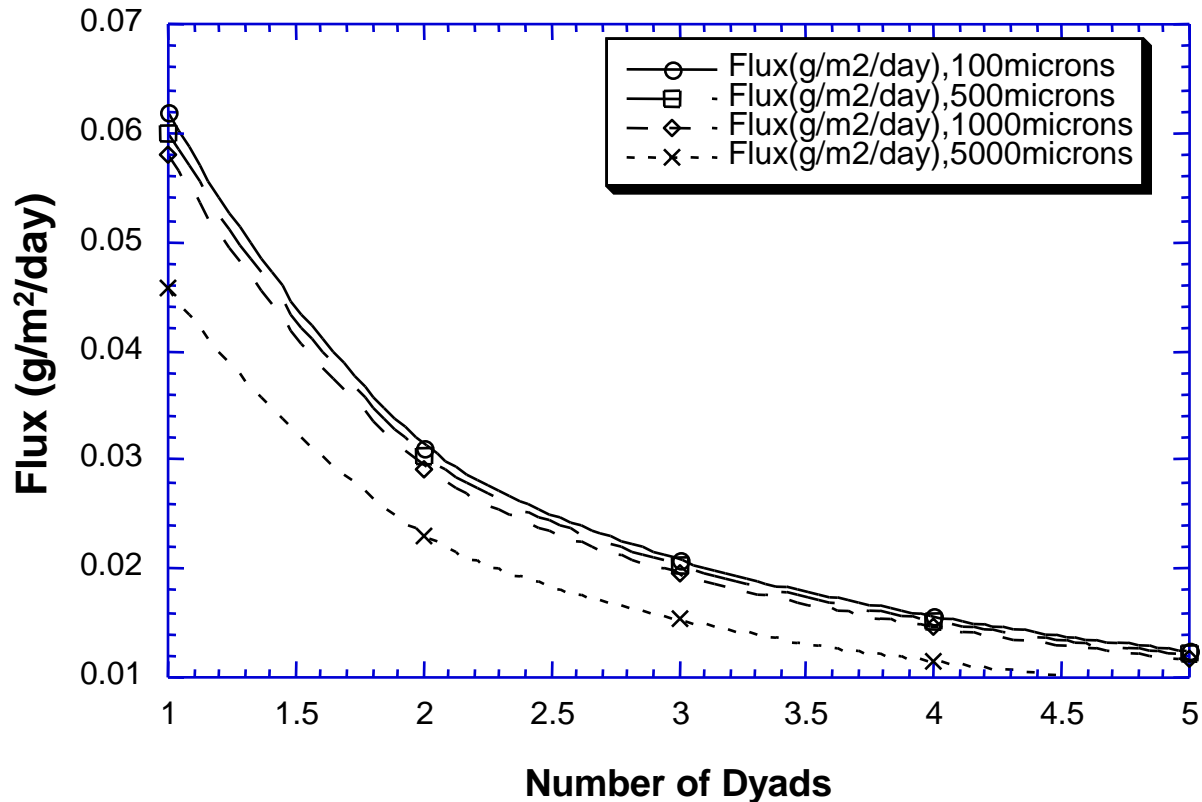
*L. Moro, et. al.,  
Flextech Workshop  
Sep. 14, 2011  
(with permission)*

# Transient (Multilayer) Regime



# Application of models to multilayer systems

*Steady state flux ( $F_{ss}$ ) calculations with varying  $D(\text{AlOx})$*



*calculated values are orders of magnitude higher than the empirical data*

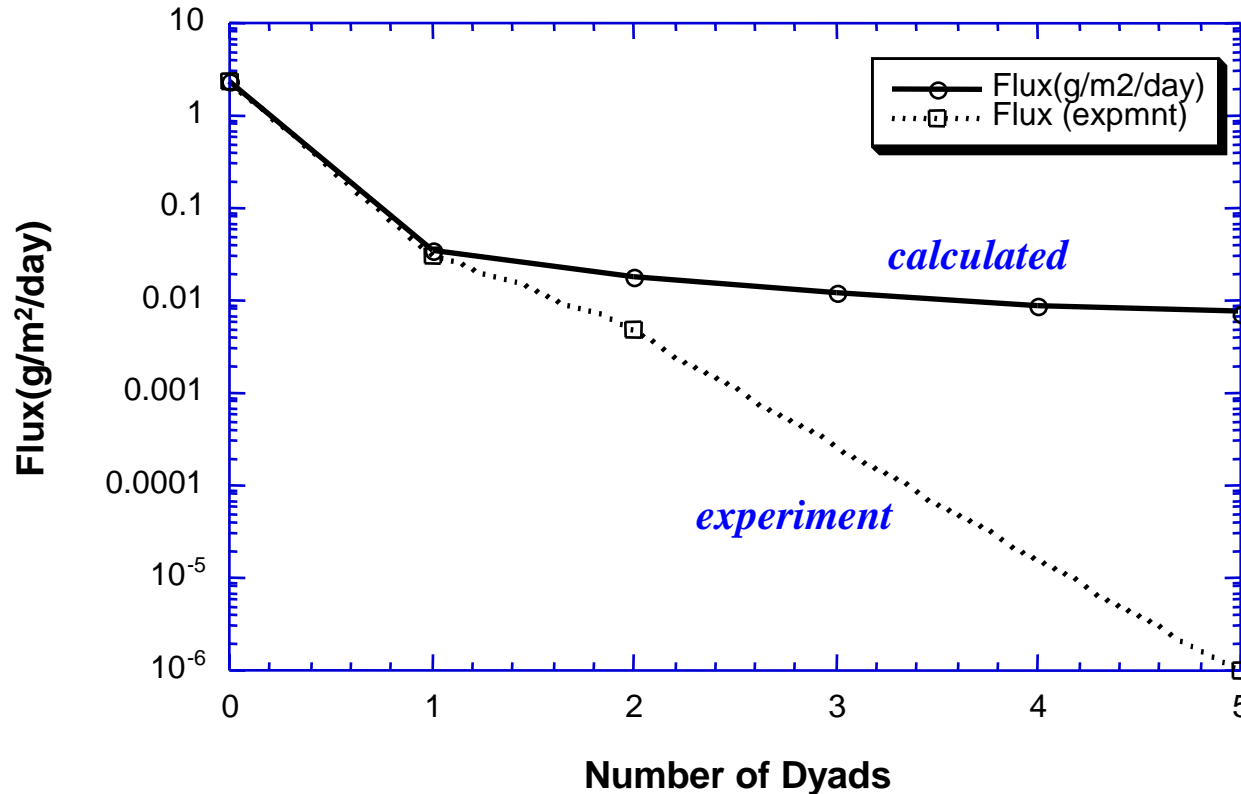


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# Application of models to multilayer systems

## *Steady state flux ( $F_{ss}$ ) calculations*

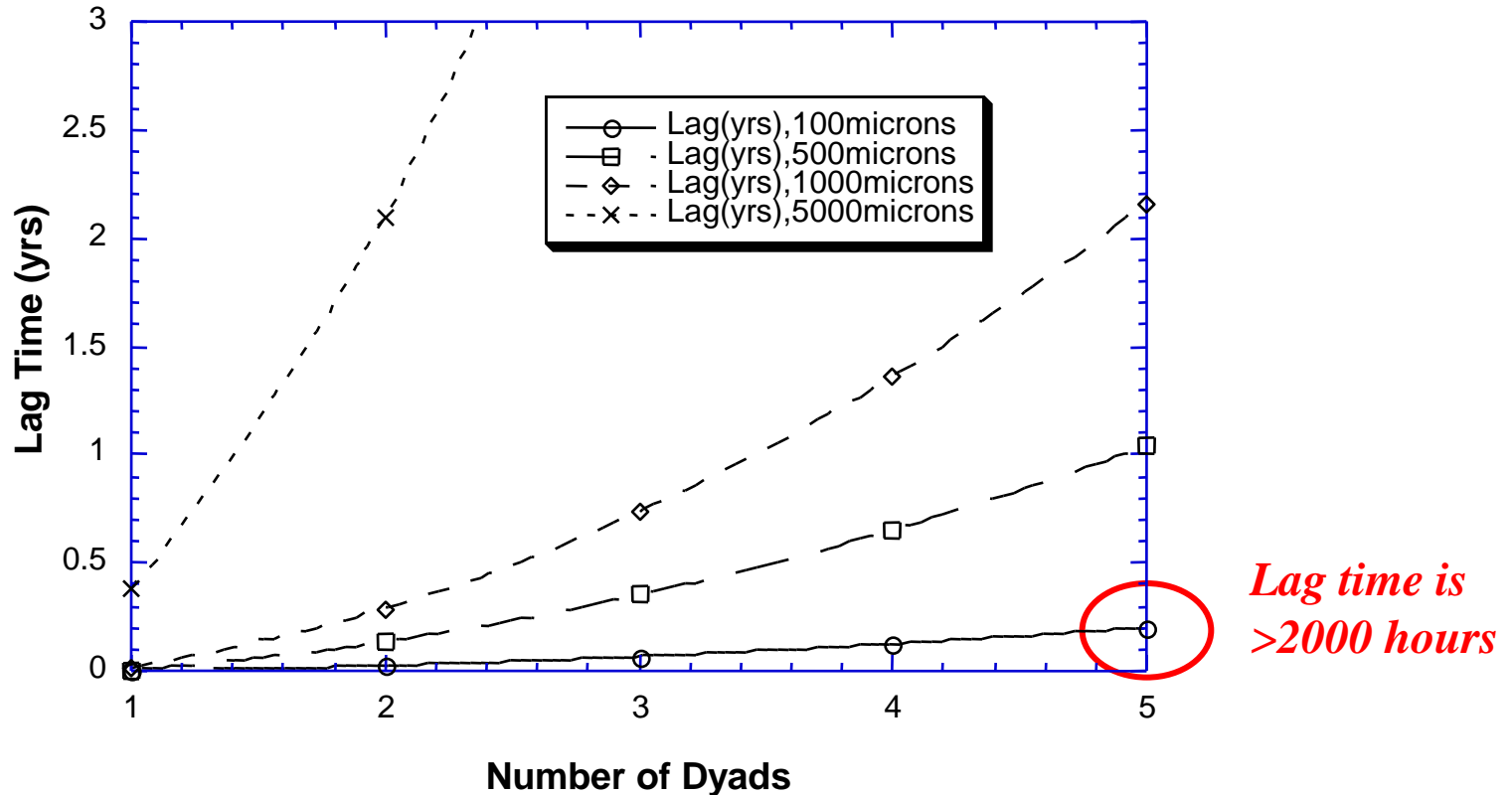


- *poor fit of models to empirical data*



# Application of models to multilayer systems

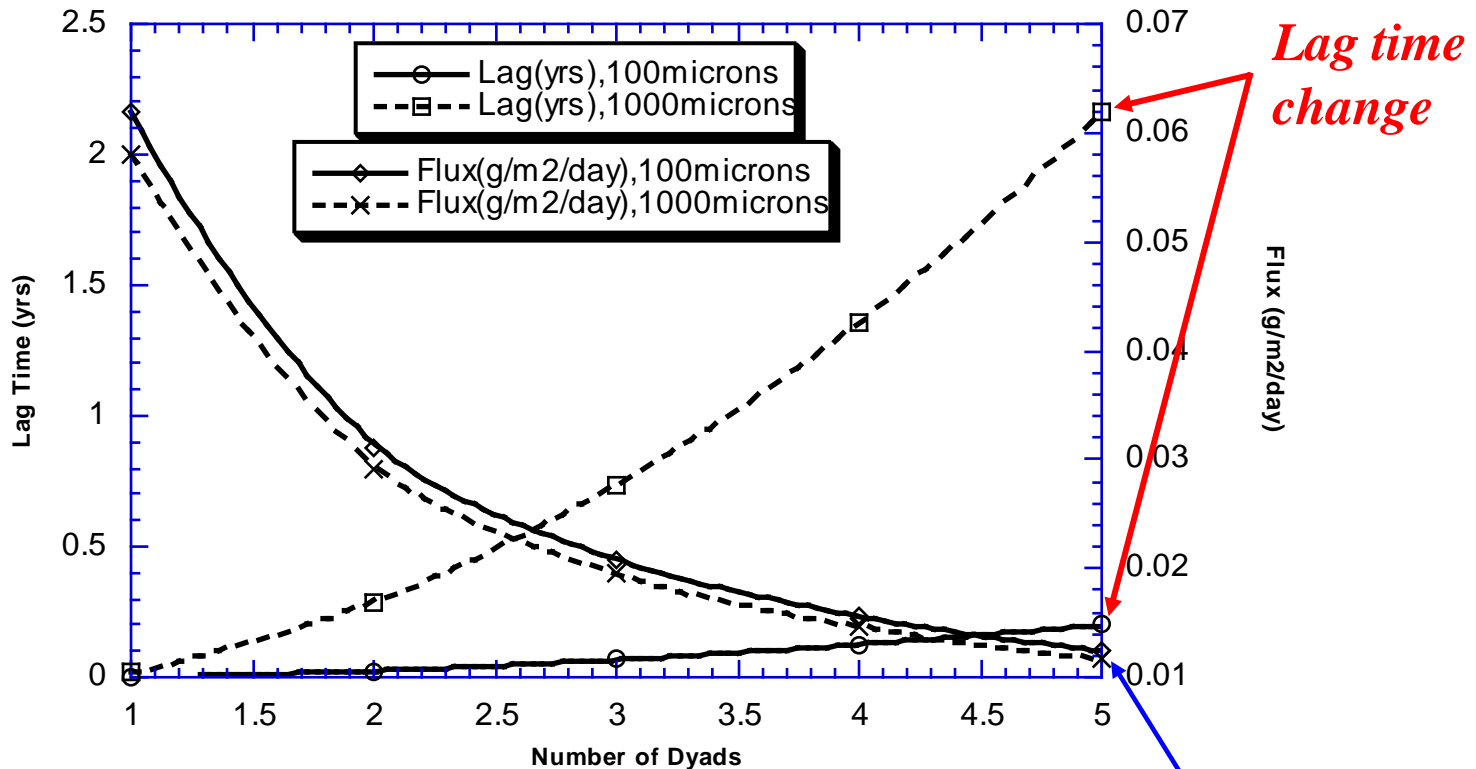
## *Lag time (L) calculations*



- *lag times are substantial (years)!*

# Application of models to multilayer systems

*Relative importance of 10x change in defect spacing on  $F_{ss}$  versus  $L$*



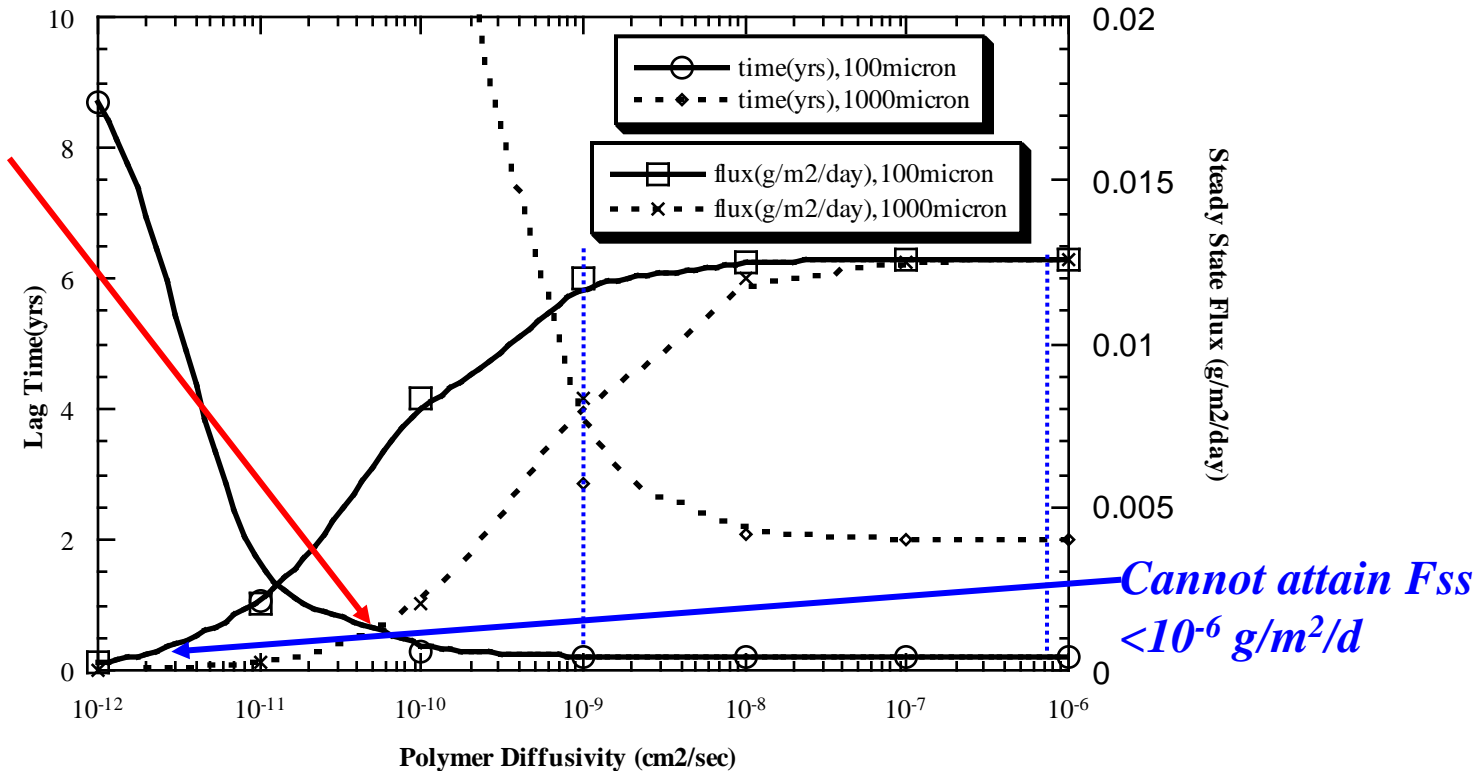
- $F_{ss}$  decreases by  $<0.005 \text{ g/m}^2/\text{d}$
- $L$  increases by  $>10x$

*Fss change*

# Polymer effects in multilayer systems

## *Polymer “D” effects – 5dyad stack*

*D < 10<sup>-10</sup>  
required to  
improve Lag  
time*

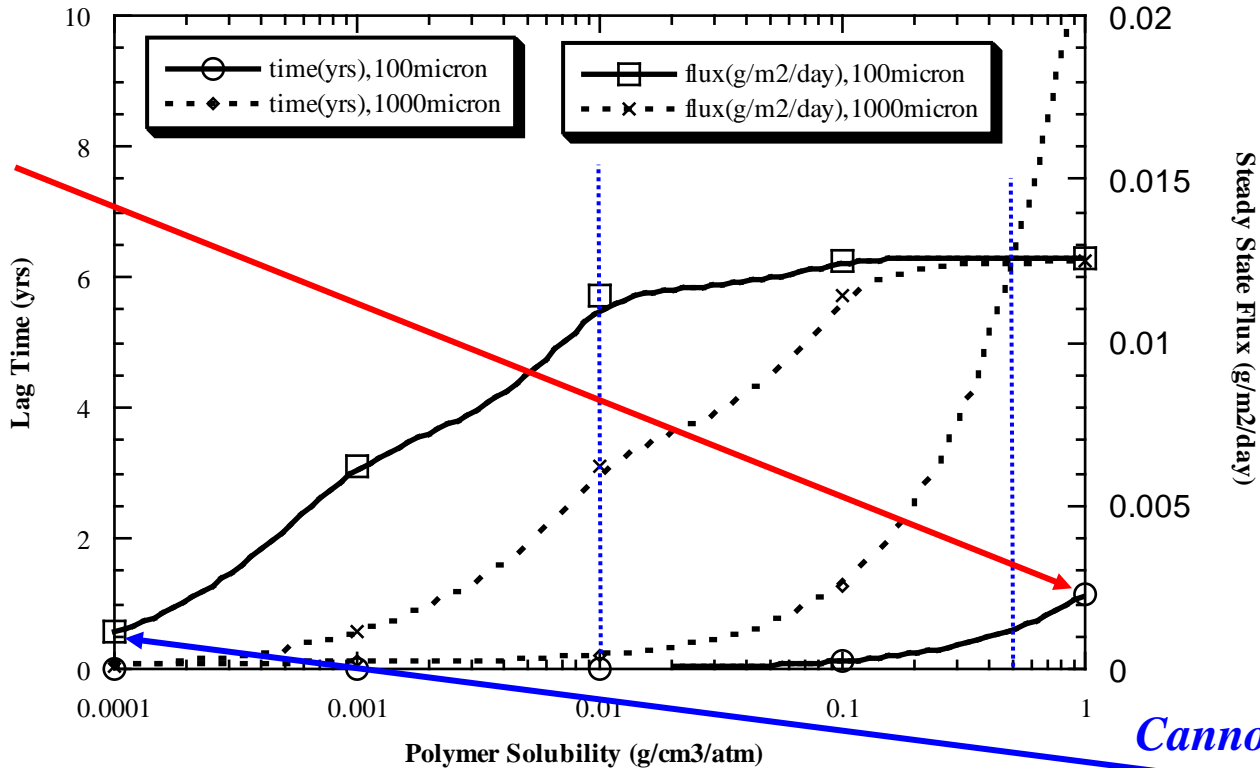


*Practical range for polymers: D = 10<sup>-9</sup> to 10<sup>-6</sup> cm<sup>2</sup>/s*

# Polymer effects in multilayer systems

## Polymer “S” effects – 5dyad stack

*S > 1.0  
required to  
improve Lag  
time*



*Cannot attain F<sub>ss</sub>  
< 10<sup>-6</sup> g/m<sup>2</sup>/d*

*Practical range for polymers: S = 0.01 to 0.5*

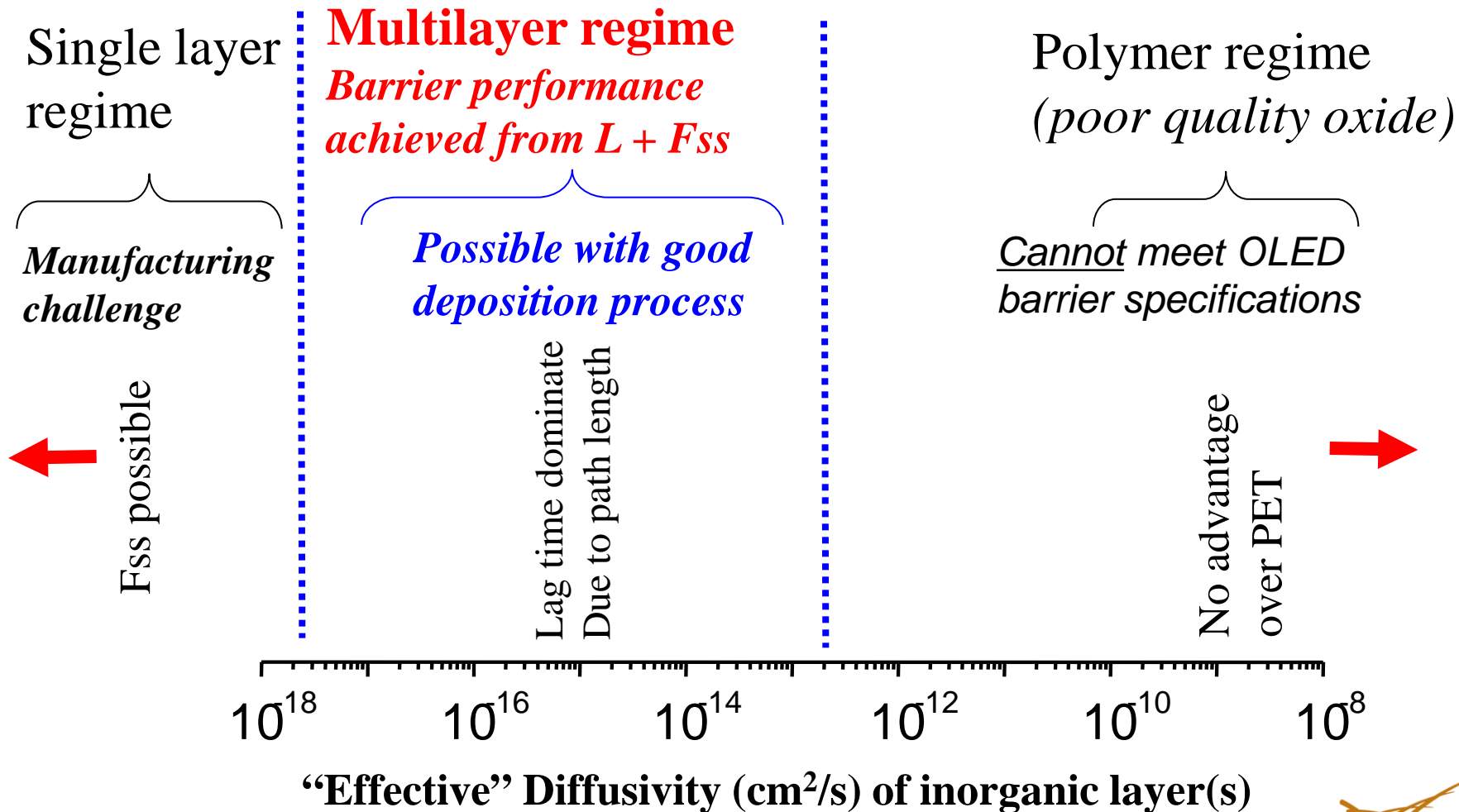
## Reported Defect Sizes and Spacings in Thin Films

Defect diameter ( $\mu\text{m}$ )	Defect density ( $\text{mm}^{-2}$ )	Defect Spacing ( $\mu\text{m}$ )	Coating material	Deposition Method	Substrate	Ref.
1.2	11-1100	30 - 300	$\text{SiO}_2$	PECVD	PET	i
1.2	5-1000	32 - 450	$\text{Si}_3\text{N}_4$	PECVD	PET	i
2.0	25-400	50 - 200	Al	evap	PET	ii
2.0	100-300	58 - 100	Al	evap	PET	iii
4-6	200	71	Al	sputtering	PET	iv
1.0-2.8	600	41	$\text{AlO}_x\text{N}_y$	sputtering	PET	v
0.8	100-1000	32 - 100	Al	evap	BOPP	vi
1.0	700	38	$\text{AlO}_x\text{N}_y$	sputtering	PET	vii

### *Construct hypothetical 5-dyad stacks using measured defect distributions*

- i. S. da Silva Sobrinho, G. Czeremuskin, M. Latrache and M. R. Wertheimer, J. Vac. Sci. Technol. A, **18**, 1, 149 (2000).
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# Thin-film Barrier “Regimes”



# Conclusions

- ▶ **High quality inorganic films *coupled* with a multilayer architecture are necessary to achieve OLED barrier requirements**
- ▶ **Lag time (transient diffusion), not steady-state flux, has a significant effect on gas permeation in these multilayer thin-film systems**
- ▶ **Consideration of steady state flux, alone, is not sufficient to describe (and predict) the performance of multilayer barrier films – must consider the transient regime**



# Implications for Manufacturing

- ▶ **Greatest gains come from improving inorganic layers (minimize defects, increase defect spacing and lower  $D_{\text{eff}}$  of  $\text{AlO}_x$  layers)**
- ▶ **Lowering the P (D&S) of the polymer (crosslinking, surface treatments, composite gradients) will improve the barrier performance**
- ▶ **Once the lag time is exceeded, the steady state flux for the multilayer systems should exceed the permeation requirement ( $F_{\text{SS}}$ ) for OLED devices**
- ▶ **Multiple polymer/inorganic layering allows use of “high-quality, manufacturable” thin-films – and does not require “near-perfect” inorganic layers**
- ▶ **Poor quality (high defect density) inorganic films cannot be used for OLED applications – even if assembled in multilayer structures**
- ▶ **Measurement of steady-state diffusion ( $F_{\text{SS}}$ ) may require testing >2000hrs**





# Future Needs

- ▶ **High rate, low cost, scalable “ultrabARRIER quality” thin-film deposition techniques**
- ▶ **More accurate predictive models – preferably ones that can use single layer/dyad validated data and predict permeation in more complex assemblies**
- ▶ **Standardized permeability measurement techniques for ultrabarriers (WVTR of  $10^{-8}$  to  $10^{-4}$  g/m<sup>2</sup>/d)**
- ▶ **Failure mechanisms (WVTR tolerance) of sensitive electronic devices (such as thin-film PV or OPV)**



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